Exhibit 5.5

Siemens Operations and Maintenance
Reliability Availability Maintenance Analysis
Operations and Maintenance
Reliability Availability Maintenance Analysis (RAM)
Taylorville Energy Center
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- Equipment specified may be different
- Automation and controls may be different

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Ram Analysis

The RAM analysis tool is a Siemens AG proprietary gasification plant configuration and RAM calculation tool. It is part of Siemens Gasification R&D development effort and is designed to calculate the equivalent plant Syngas output based on plant configuration, typical process redundancies, component reliability and plant maintenance schedules.

Reliability is defined as the ability of a plant, system or component to perform its required functions under stated conditions for a specified period of time. Reliability does not consider the time in which the system can not perform its functions because of scheduled maintenance. Availability is the ratio of (a) the total time a functional/ reliable system is capable of being used during a given interval to (b) the length of the interval. This ratio includes the time the system is not available because of forced downtime and scheduled maintenance.

The plant reliability is calculated with the help of Failure Mode Effect Analysis (FMEA), Markov models, operation and maintenance experience, published component reliability and system information.

The reliability of a gasification system strongly depends on the quality of the detailed design, the controls philosophy and the selection of the most reliable components. This RAM analysis is not based on a specific detailed design but it is based on the assumption that the detailed design is guided by prudent design principles and component selection. An implemented Monte Carlo simulation of the RAM calculation improves the quality of RAM tool results. We regard this RAM simulation software as an important tool to assess the design quality in regards to RAM.

The maintenance plans used in the model reflect generic data with some maintenance assumptions obtained from Tenaska for scheduled maintenance and reflects typical component manufacturer information, system and maintenance experience. Availability improvements can be achieved when the final design is complete. The annual maintenance plans will have to be adjusted to the actual systems design (e.g.: train redundancy) and to the requirements of plant components selected. The analysis is based on some assumptions of efficiency in the completion of any potential scheduled maintenance during the forced outages times. The following assumptions are being used:

- The planned gasifier burner and coal island inspections are managed during unplanned outages.
- The ASU planned maintenance cycles will be scheduled within the overall facility shutdown on 3 year intervals.

The RAM tool is designed to calculate the reliability factor and the equivalent availability of the stable system when it is fully commissioned. During the first years of operation the plant stability must be improved by debugging and system improvements. This tool can not reflect on the quality of the process design, plant construction & commissioning or the O&M team. Therefore a learning and improvement period has to be applied with reduced plant reliability for the first years of plant operation. Past experience from the startup of IGCC plants indicate that a learning curve can be expected. Compared to first generation IGCC plants (Figure 1), second
generation IGCC data (Figure 2) show an improvement in the learning curve. This second generation plant is a heavy liquid IGCC plant located in Italy. Since Taylorville is a coal plant an improvement between the early coal IGCC and the second generation Oil fired IGCC could be expected. For the Taylorville Energy Center in Taylorville, IL, the plant availability for the first and second year of operation is assumed to be in the range of 55-65% for the first and 75-85% for the second year of operation. The following years are calculated based on the calculated system reliability and scheduled maintenance requirements.

Siemens Energy Service has developed close relationships with the following leading component and system suppliers to cooperate during the RAM tool development phase and to validate the results of the RAM calculation tools.

Siemens Fuel Gasification, D          Coal Gasification and Syngas scrubbing
Johnson Matthey, UK             CO-Shift, COS Hydrolysis, Methanzation
Claudius Peters, D                Coal Milling and Drying
Siemens Energy, D                ASU Compressors
Red Mountain Energy             ASU plant
Linde, D                     ASU, AGR
Williams Crusher, US        Coal Milling and drying and conveying
Siemens Energy            Controls
Plant Layout

The RAM model for this project is based on the following assumed plant layout:

![Plant Layout Diagram]

Plant Configuration
Module: | Included in RAM calculation:
--- | ---
Gasification | Yes
Milling | Yes
ASU | Yes
COS_Hydrolysis | No
CO-Shift | Yes
Methanation | Yes
Rectisol | Yes
Claus Plant | Yes

**Detail Plant Description (Input)**

**Gasification Systems**
Gasifiers 2
Blackwater systems 1
Capacity of Blackwatersytems (Gasifiers) 2
Necessary number of Gasifiers at 100% for Total Output of 100% of the Gasification System 2

**Milling and Drying**
Number of Silos
Pulverized Coal 2
Number of Coal Mills 2
Necessary Mills Working per silo: 1
Capacity of Silo Pulverized Coal (h) 8
Capacity of Silo Raw Coal (h) 12

**ASU**
Number of ASU Modules for 100% capacity 1
Oxygen Storage 24h

**CO Shift**
Number of Shift Modules 1

**COS Hydrolysis**
Number of Hydrolysis Modules

**AGR Rectisol**
Number of Absorption Lines 1
Number of Regeneration Lines 1
Capacity of a 1
Regeneration Line

**Sulfur Treatment Plant**
Number of
Claus Plants 2
Number of Tail Gas Treatment 2
Capacity of TGT 1

**Methanation**
Number of
Methanation Modules** 1

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**RAM Calculation Results for the Gasification Plant**

<table>
<thead>
<tr>
<th>Observation Period (years)</th>
<th>12</th>
</tr>
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<tbody>
<tr>
<td>Year 1</td>
<td>55-65%*</td>
</tr>
<tr>
<td>Year 2</td>
<td>75-85%*</td>
</tr>
<tr>
<td>Year 3</td>
<td>86.0%</td>
</tr>
<tr>
<td>Year 4</td>
<td>86.0%</td>
</tr>
<tr>
<td>Year 5</td>
<td>86.0%</td>
</tr>
<tr>
<td>Year 6</td>
<td>85.1%</td>
</tr>
<tr>
<td>Year 7</td>
<td>86.1%</td>
</tr>
<tr>
<td>Year 8</td>
<td>86.0%</td>
</tr>
<tr>
<td>Year 9</td>
<td>80.3%</td>
</tr>
<tr>
<td>Year 10</td>
<td>85.9%</td>
</tr>
<tr>
<td>Year 11</td>
<td>85.9%</td>
</tr>
<tr>
<td>Year 12</td>
<td>85.2%</td>
</tr>
</tbody>
</table>

Average estimated annual equivalent available output over 10 years after shake down period.
(Includes forced and scheduled outages)

85.2 % of Total Output

*Learning curve and system improvement period
IGCC Availability History
excludes operation on back-up fuel

Baseline Study

Source: EPRI

Figure 1
IGCC AVAILABILITY

Plant Start-up in 2000. IGCC availability has increased due to the technical improvements and to the O&M management optimisation.

<table>
<thead>
<tr>
<th>Year</th>
<th>Availability</th>
</tr>
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<tbody>
<tr>
<td>2001</td>
<td>78.1%</td>
</tr>
<tr>
<td>2002</td>
<td>88.1%</td>
</tr>
<tr>
<td>2003</td>
<td>91.4%</td>
</tr>
<tr>
<td>2004</td>
<td>90.0%</td>
</tr>
<tr>
<td>2005</td>
<td>90.0%</td>
</tr>
<tr>
<td>2006</td>
<td>92.5%</td>
</tr>
<tr>
<td>2007</td>
<td>91.5%</td>
</tr>
</tbody>
</table>

NOTE: Plant availability includes also the scheduled shutdown.

Figure 2